

# Supersonic Nozzle Design & Performance Analysis

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Application:

Commercial Sea Level  
Rocket

QoI #1:

Thrust Coefficient

QoI #2:

Specific Impulse

# Synthesis

| Aspects of Engineering             | Pros                                                                                                          | Cons                                                                                                       |
|------------------------------------|---------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------|
| Experiments (Supersonic tunnel)    | Captures real physics, shows transient behavior / expansion (under, over, or perfect)                         | Data is mostly qualitative, limited internal flow data, sensitive to setup conditions                      |
| Theory (Quasi-1D)                  | Fastest tool, replicable, steady state quick predictions of $p$ , $T$ , $\rho$ , $M$ , etc,                   | Carries several assumptions (steady state, 1D, idealized), can not capture 2D shocks or transient behavior |
| Computational Fluid Dynamics (MFC) | Validate flow structure beyond 1D metrics, applicable to transient observation (validating nozzle robustness) | Time consuming, computationally intensive, model assumptions can produce unrealistic results               |

## Key Takeaways from FPC P1 / 2:

- Quasi-1D steady theory is best for optimization of geometry because nozzles can be directly compared at the same conditions without time-dependent (transient) conditions muddying results.
- Experiments and MFC are best for observing flow physics → Transient tools show what is happening physically, and speak to the robustness of our design (how it operates in startup, shutdown, states outside intended conditions), while steady-state models tell us what geometry is best under specific conditions (determined by our application).

# Quantities of Interest

## Thrust Coefficient

$$C_F = \frac{F}{p_c A_t}$$

Measures nozzle efficiency independent of size (scales up and down)

## Specific Impulse

$$I_{sp} = \frac{C_F \cdot c^*}{g}$$

Measures how much thrust is produced per unit of propellant consumed

## Qols Considered <sup>1,2,3</sup>

1. Thrust
2. Thrust Coefficient
3. Mass flow
4. Specific Impulse
5. Exit Pressure
6. Ambient Pressure
7. Nozzle Efficiency

## Takeaways

1. Both are maximized simultaneously due to their linear relationship
2.  $C_F$  is sensitive to wall angle and area ratio, thus optimizing relationship is important
3. Well-optimized design point gives you the best average performance across the full ascent, not just at one moment

[1] Tuttle, Perfect Bell Nozzle Parametric and Optimization Curves (NASA, 1983)

[2] Jones et al., Proposed Flight Research of a Dual-Bell Rocket Nozzle System to Enhance NASA's Space Launch System Performance (NASA, 2013)

[3] Kacynski et al., The Prediction of Nozzle Performance and Heat Transfer in Rocket Engines (NASA, 1994)

# Nozzle Geometries

## Geometry #1: Bell <sup>1</sup>

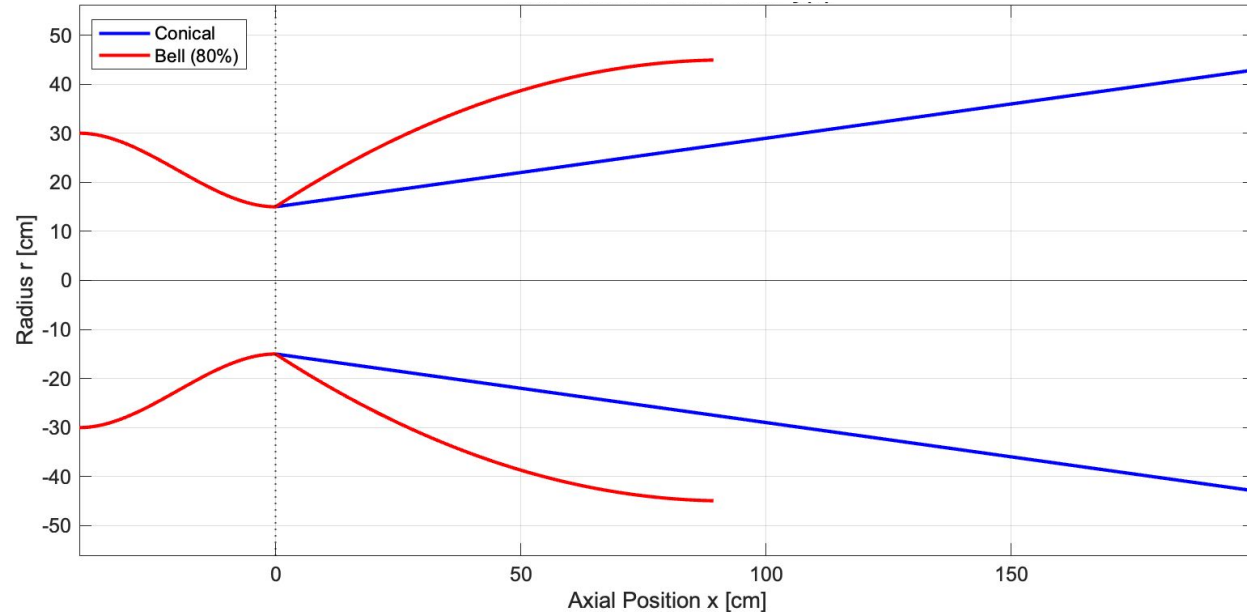
$$y(x) = ax^2 + \tan(\theta_N)x + r_t$$

Diverging section with parabolic wall profile where wall angle decreases continuously

## Geometry #2: Conical <sup>2</sup>

$$y(x) = r_t + \tan(\alpha)x$$

Diverging section with straight wall profile



[1] "Rocket Nozzles: Types, Manufacturing & Materials," Astroforge Tech. Available: <https://astforgetech.com/rocket-nozzles-types-manufacturing-materials/>

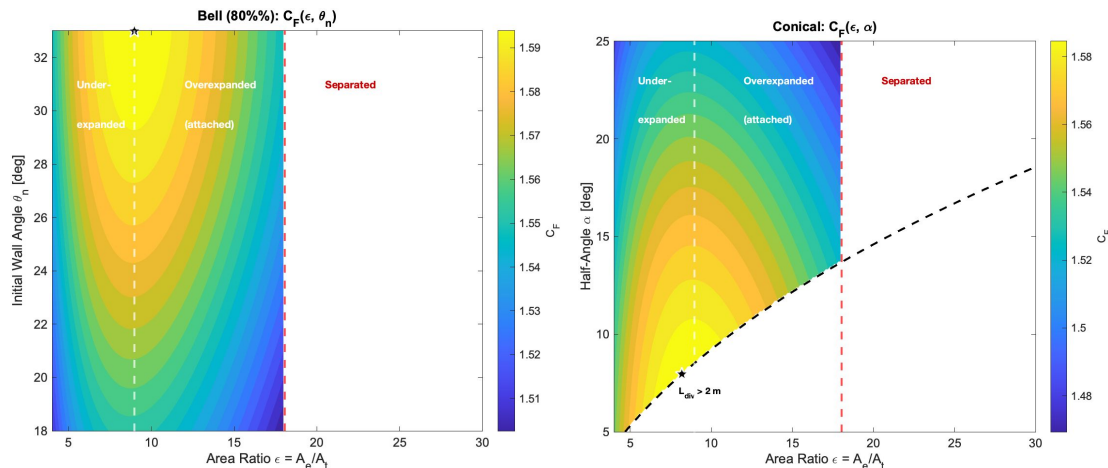
[2] G. V. R. Rao, "Exhaust Nozzle Contour for Optimum Thrust," Jet Propulsion, 1958. Available: <https://www.semanticscholar.org/paper/Exhaust-Nozzle-Contour-for-Optimum-Thrust-Rao/230e0a17e1a07550212b65f99f7e46aac59811ae>

[3] Dieter K. Huzel and David H. Huang, Modern Engineering for Design of Liquid-Propellant Rocket Engines. American Institute of Aeronautics and Astronautics

# Parameter Space and Performance

## Optimization Results

|                     | Parameter                          | Conical              | Bell (80%)                                    |
|---------------------|------------------------------------|----------------------|-----------------------------------------------|
| <i>Optimization</i> | Area ratio $\varepsilon = A_e/A_t$ | 8.18                 | 8.96                                          |
|                     | Shape angle                        | $\alpha = 8.0^\circ$ | $\theta_N = 33.0^\circ, \theta_E = 1.2^\circ$ |
| <i>QoIs</i>         | Thrust coefficient $C_F$           | 1.590                | 1.598                                         |
|                     | Specific impulse $I_{sp}$ [s]      | 287.5                | 289.0                                         |
| <i>Engineering</i>  | Diverging length $L_{div}$ [m]     | 1.997                | 0.893                                         |
|                     | Thrust $F$ [kN]                    | 786.9                | 790.9                                         |

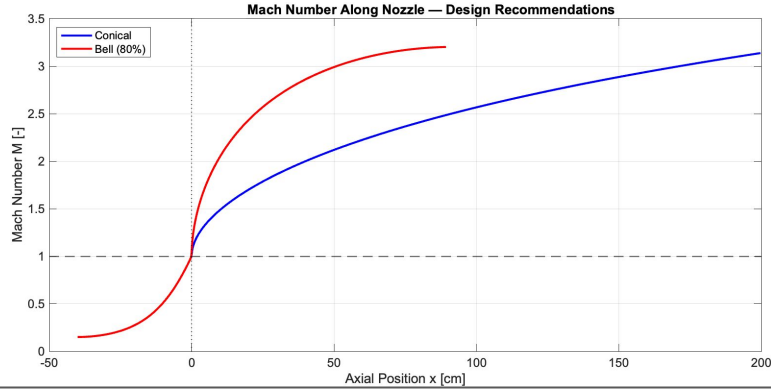


## Initial Conditions<sup>1</sup>

| Parameter                 | Symbol    | Value   | Units  |
|---------------------------|-----------|---------|--------|
| <i>Gas properties</i>     |           |         |        |
| Ratio of specific heats   | $\gamma$  | 1.25    | —      |
| Specific gas constant     | $R_g$     | 355.4   | J/kg·K |
| <i>Chamber conditions</i> |           |         |        |
| Stagnation pressure       | $p_c$     | 6.89    | MPa    |
| Stagnation temperature    | $T_c$     | 3533    | K      |
| <i>Ambient conditions</i> |           |         |        |
| Atmospheric pressure      | $p_{atm}$ | 101.325 | kPa    |
| <i>Fixed geometry</i>     |           |         |        |
| Throat radius             | $r_t$     | 0.15    | m      |
| Max diverging length      | $L_{max}$ | 2.00    | m      |

[1] "SpaceX Unveils Plans To Be World's Top Rocket Maker. Available: <https://web.archive.org/web/20150621134912/http://aviationweek.com/awin/spacex-unveils-plans-be-world-s-top-rocket-maker>

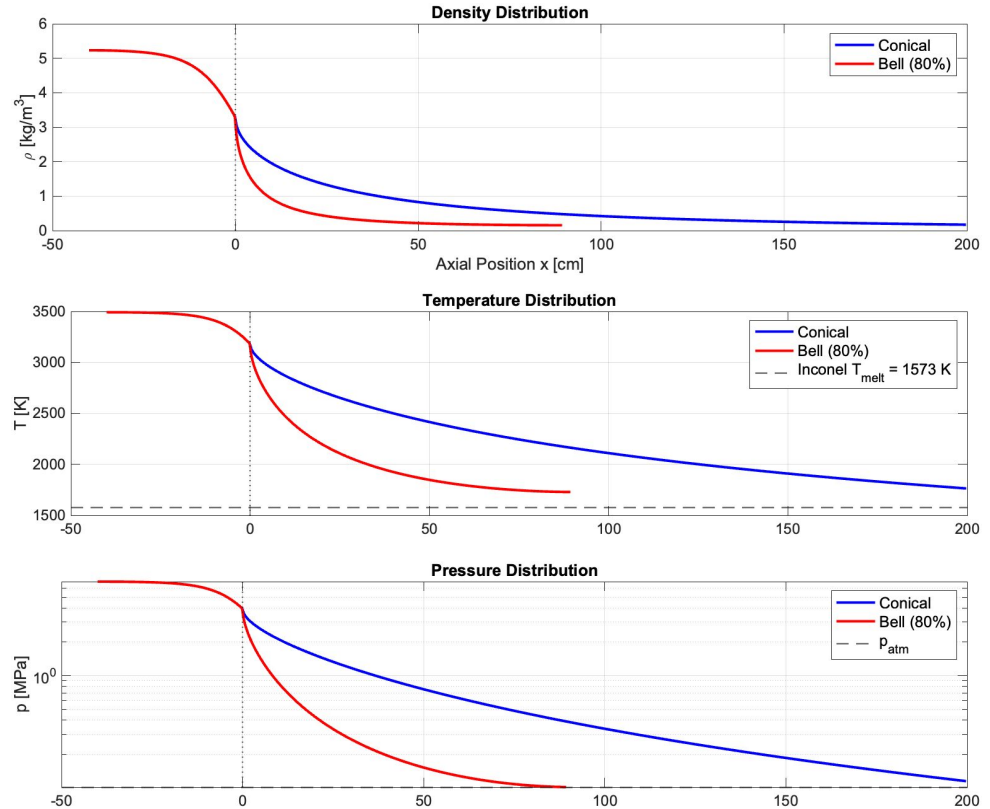
# Ideal Performance



|                 |                                   |             |       |
|-----------------|-----------------------------------|-------------|-------|
| Flow properties | Exit Mach number $M_e$            | 3.138       | 3.202 |
|                 | Exit pressure ratio $p_e/p_{atm}$ | 1.131       | 1.001 |
|                 | Throat temperature $T^*$ [K]      | 3182 (both) |       |
|                 | Exit temperature $T_e$ [K]        | 1764        | 1728  |

Bell beats conical by **+0.51%** in  $C_F$  and **+1.5s** in  $I_{sp}$  at **55%** shorter length.

Throat temperature reaches **3182K**, but Inconel 718 melts at **1573K**<sup>[1]</sup>, thus wall would vaporize. We propose using regenerative cooling, which pumps cold fuel through wall channels before combustion to lower wall temperature.



[1] M. Abdullah K., Kavyassree G., and Srimathi S., "Comparative Analysis of Inconel 718 and Inconel 625 for Rocket Nozzles: Performance, Durability, and Manufacturing Influence," Acceleron Aerospace Journal, vol. 4, no. 3, 2025. Available: <https://acceleron.org.in/index.php/aaaj/article/view/227>

# Recommendations

## Overall Recommendation:

Bell Shaped Nozzle with the following form:

$$y(x) = -0.3521 x^2 + \tan(33^\circ) x + 0.15$$

The 80% bell shaped nozzle achieved higher  $C_F$  and  $I_{sp}$  at less than half the diverging length of the equivalent conical design.

## Final Geometry

|                                    |         |
|------------------------------------|---------|
| Area ratio $\varepsilon = A_e/A_t$ | 8.96    |
| Initial wall angle $\theta_N$      | 33.0°   |
| Exit wall angle $\theta_E$         | 1.2°    |
| Diverging length $L_{div}$         | 0.893 m |
| Exit radius $r_e$                  | 0.449 m |

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## Recommendations and Reflections

1. The bell outperformed conical by only +0.51% in  $C_F$ , so maybe area ratio dominates performance at this pressure and wall shape is a secondary factor
2. Model how thrust changes at various altitudes, since our optimizer only finds the best design at one fixed altitude
3. Run 2D fluid simulations on the optimal bell nozzle to check how much real-world losses like friction and shocks reduce performance below our theoretical predictions

# Contributions

**Peyton Marcotte:** Writing, Original Draft (lead), Visualization (equal).

**Logan Suryamega:** Formal Analysis (lead), Writing, Review, and Editing (equal).

**Juan Perez:** Data Collection (lead), Software / Code (equal).

All authors reviewed and approved the final submission.

# MATLAB Code

<https://drive.google.com/file/d/1YCLF879lo6ygF7tXPoS7pFwbMpb3-xpC/view?usp=sharing>